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2025-04-08

Proposed changes to the calculation of $SFP_{int-limit}$ for NRVUs in the revised Regulation (EU) 1253/2014

In a nutshell

With this position paper, members of the Eurovent Product Group 'Air Handling Units' point out the identified concerns regarding the calculation of the $SFP_{int-limit}$ in the current proposal recommended for adoption in the revised regulation and propose modification aiming at:

- **Eliminating an excessive increase of $SFP_{int-limit}$ at high energy recovery efficiency.**
- **Providing the same $SFP_{int-limit}$ bonus due to a higher actual $\eta_{e,nrvu}$ than the minimum limit regardless of the design outdoor temperature.**

Introduction

The follow-up study consultant recommended in its [Phase 1.1: Technical Analysis \(Draft\)](#)¹ document to accept the new 'known/unknown place of installation' approach for $\eta_{e,nrvu,min}$ and $SFP_{int-limit}$. It was also recommended to adopt in the revised regulation the suggested by Eurovent changes to formulas as outlined in Section 1.4 of [PP – 2021-04-30](#)². These recommendations were very much appreciated by Eurovent members.

However, in further analysing the impact and practical implementation of the proposed new formulas, we have encountered significant issues that we believe require further attention and modification. The identified issues, proposed changes and detailed clarifications are presented in the following sections.

Identified issues

When examining the formulas, we have noticed that the current proposal for the correction factor (E) which allows an additional SFP_{int} limit if the actual efficiency of energy recovery ($\eta_{e,nrvu}$) is higher than $\eta_{e,nrvu,limit}$ for a given design outdoor temperature (ODA), results in very high E-factor values (going to infinity) at high actual efficiencies (above approximately 85%, which can be easily achieved by available technology).

$$E = \frac{\eta_{e,act}}{1 - \eta_{e,act}} \cdot \frac{1 - \eta_{e,ref}}{\eta_{e,ref}}$$

This is incorrect from the perspective of the coefficient of energy recovery performance (ε), which in this case can be defined as a ratio between the additional heat gain (due to higher efficiency) and the additional maximum additional fan power.

$$\varepsilon = \frac{\Delta\Phi_{HRC}}{\Delta SFP_{int-limit}}$$

¹ <https://eco-ventilation-review.eu/wp-content/uploads/2024/06/Ventilation-Study-Phase-1.1-Technical-Analysis-Final-for-Upload-June-2024.pdf>

² <https://www.eurovent.eu/wp-content/uploads/position-papers-files-public/pp-2021-04-30-eurovent-comments-on-draft-revised-eu1253-and-eu1254-1.pdf>

With increasing efficiency this coefficient tends to zero, which contradicts the similar concept of the heat pump performance efficiency.

Furthermore, we have noticed that with the current E-factor function, additional limit for SFP_{int} depends on the design outdoor temperature. This means that a unit with a high energy recovery efficiency installed in cold climate would have to meet a more stringent $SFP_{int-limit}$ than the same unit installed in warm climate. In the opinion of Eurovent members, the $SFP_{int-limit}$ bonus for a higher energy recovery efficiency should be the same regardless of the place of installation.

The issues raised are illustrated in Diagram 1.

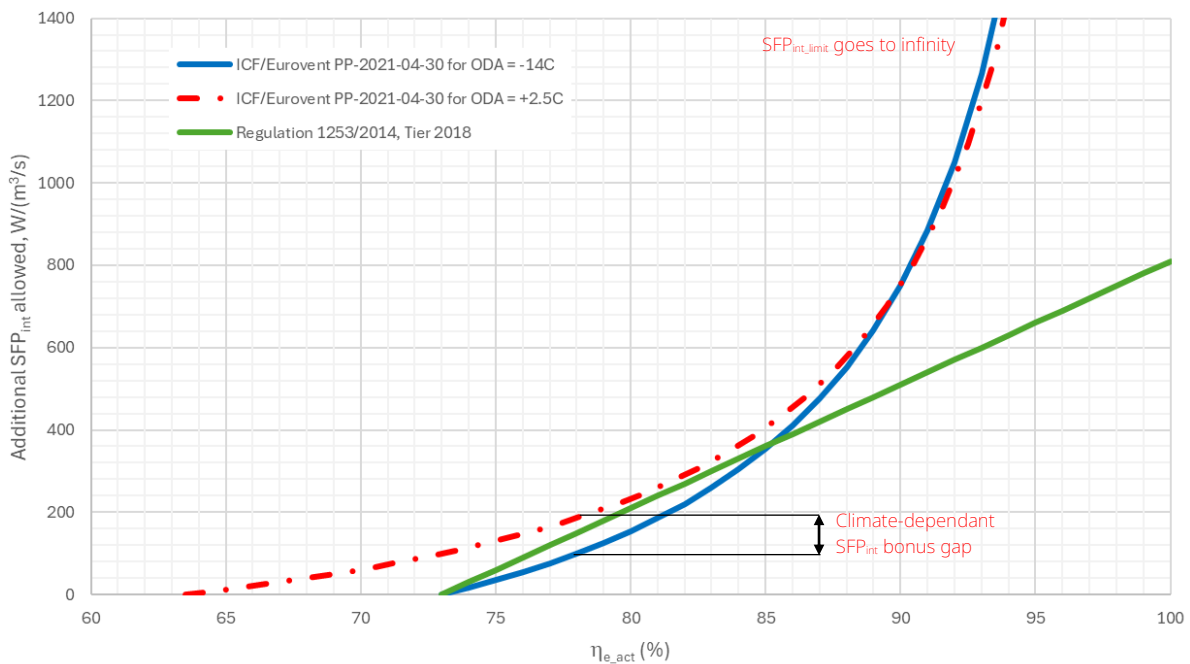


Diagram 1. Additional SFP_{int} limit for different ODA temperatures and the SFP_{int} bonus gap. Data refers to: other ERC type (without moisture recovery), $q_{nom} > 2 \text{ m}^3/\text{s}$, $C = 1$, $F_{sup} = 150$ (ISO ePM1 >50% \approx F7), $F_{exh} = 120$ (ISO ePM10 >50% \approx M5)

Proposed modifications

To eliminate the pointed issues, while maintaining unchanged the overall concept of the new approach based on Dr Kaup's original study, we propose the following:

- Adjust (decrease gradient) the function of the correction factor E for high efficiency values.
- Calculate $SFP_{int-limit}$ as a function of the actual $\eta_{e,nrvu}$ and not the design outdoor temperature to exclude the influence of climate.
- Adjust the $SFP_{int-limit}$ function so that for a unit without any controls ($C = 1$), it gives limits approx. 10% lower than the current 2018 values, and for a unit with controls corresponding to $C = 1.1$, it gives the same limits as the current 2018 values.

In addition, to facilitate the implementation of the new approach, we propose to simplify the set of formulas by embedding both the $SFP_{HRS-base}$ and E into the following single equation for $SP_{int-limit}$ with coefficients depending on the range of nominal air flowrate (q_{nom}) and the type of energy recovery system:

$$SFP_{int_limit} = 0.95 \cdot C \cdot (a \cdot \eta_{e_nr\ddot{u}_act}^2 + b \cdot \eta_{e_nr\ddot{u}_act} + c + F_{sup} + F_{exh}) \quad \text{if } q_{nom} \geq 2 \text{ m}^3/\text{s}$$

$$SFP_{int_limit} = 0.95 \cdot C \cdot (a \cdot \eta_{e_nr\ddot{u}_act}^2 + b \cdot \eta_{e_nr\ddot{u}_act} + c - 140 \cdot q_{nom} + F_{sup} + F_{exh}) \quad \text{if } q_{nom} < 2 \text{ m}^3/\text{s}$$

Where:

- $\eta_{e_nr\ddot{u}_act}$ - actual efficiency of energy recovery, %-points
- C, F_{sup}, F_{exh} - the same and unchanged factors as in the previous documents^{1,2}
- a, b, c - coefficients given in Table 1

Energy recovery system	Nominal air flow rate q_{nom}	Parameters of the polynomial		
		a	b	c
run-around HRS	$\geq 2 \text{ m}^3/\text{s}$	0.794	-82.6	2892
	$< 2 \text{ m}^3/\text{s}$	0.794	-82.6	3172
moisture HRS	$\geq 2 \text{ m}^3/\text{s}$	0.794	-93.7	3043
	$< 2 \text{ m}^3/\text{s}$	0.794	-93.7	3323
other HRS	$\geq 2 \text{ m}^3/\text{s}$	0.794	-90.6	2864
	$< 2 \text{ m}^3/\text{s}$	0.794	-90.6	3144

Table 1. Parameters for the polynomials for different ERS and air flow ranges.

Effect of proposed modifications

With the proposed new formulas:

- Up to a temperature efficiency of around 85% the SFP_{int_limit} increases exactly as in the previous proposal and then continues to increase at a low gradient.
- The additional SFP_{int_limit} value due to a $\eta_{e_nr\ddot{u}_act}$ higher than the $\eta_{e_nr\ddot{u}_limit}$ is the same regardless of the outdoor design temperature
- The SFP_{int_limit} for the ODA temperature-dependent $\eta_{e_nr\ddot{u}_limit}$ is 10% lower than the current 2018 limit for a unit without any controls ($C = 1$) and the same as current 2018 limit for a unit with controls corresponding to $C = 1.1$.
- The maximum pressure drop associated with the energy recovery system (on both sides) corresponds much better to the actual performance of the available technology.

These effects are illustrated in Diagram 2 and Diagram 3 below.

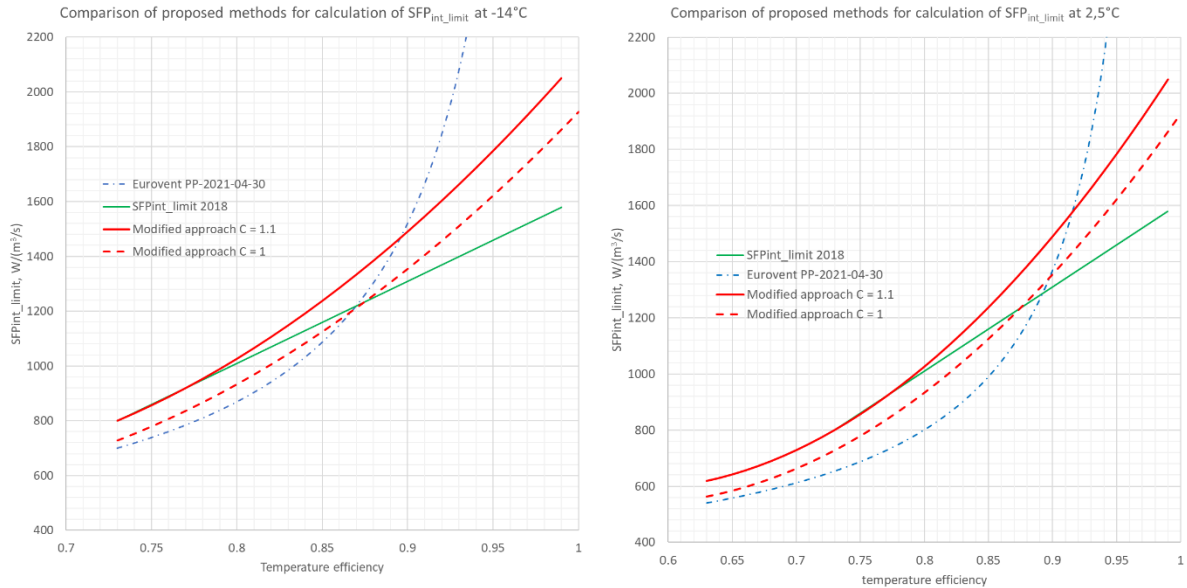


Diagram 2. Comparison of SFP_{int_limit} for the new modified approach, the previous proposal and the current Regulation for outdoor temperature of $-14^{\circ}C$ and $+2.5^{\circ}C$. Data refers to: other ERC type (without moisture recovery), $q_{nom} > 2 \text{ m}^3/s$, $F_{sup} = 150$ (ISO ePM1 >50% $\approx F7$), $F_{exh} = 135$ (ISO ePM2.5 >50%)

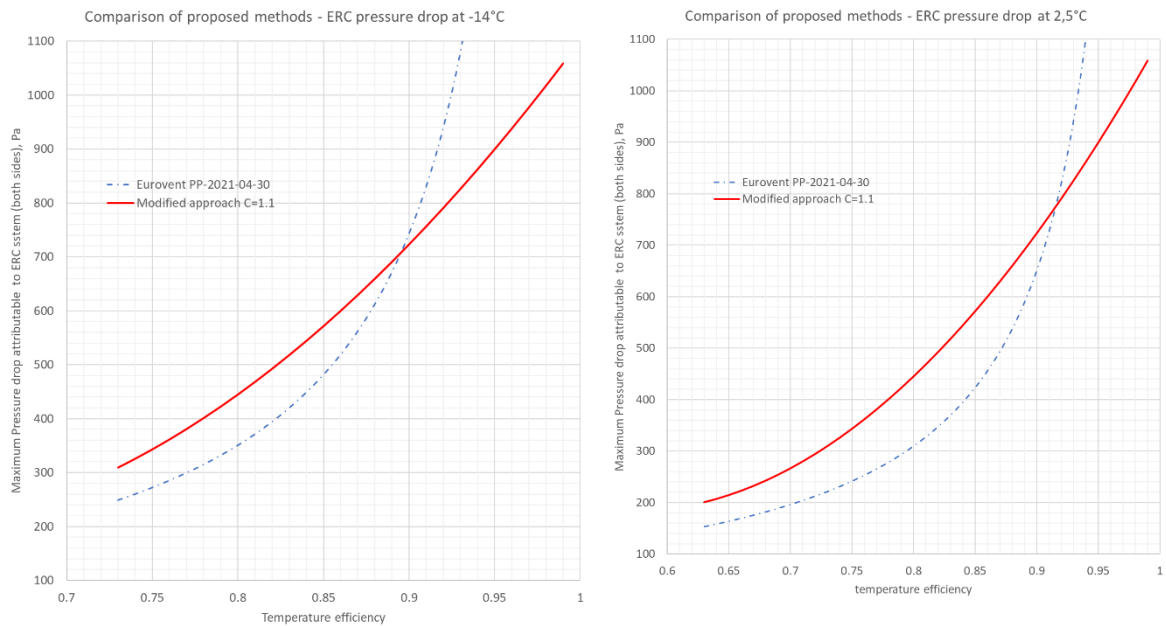


Diagram 3. Comparison of maximum pressured drop attributable to the energy recovery system (both sides) for the new modified approach and the previous proposal for outdoor temperature of $-14^{\circ}C$ and $+2.5^{\circ}C$. Data refers to: other ERC type (without moisture recovery), $q_{nom} > 2 \text{ m}^3/s$, $F_{sup} = 150$ (ISO ePM1 >50% $\approx F7$), $F_{exh} = 135$ (ISO ePM2.5 >50%), total efficiency of the fans = 60%, $C = 1.1$

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